

Development of fatigue cracks from mechanically machined scratches on 2024-T351 aluminium alloy-Part I: experimentation and fractographic analysis

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Abstract

Clad and unclad 2024-T351 aluminium alloy sheets, weakened by mechanically machined scratches, were fatigued to investigate the effect of small surface damage, like scribe marks, on aircraft fuselage joints. The role of scratch cross section geometry on fatigue life of scribed components was analysed. Scratches between 25 and 185 μm deep, with 5, 25 and 50 μm root radii were cut on samples surface using diamond tipped tools. After testing fracture surfaces were examined using a SEM and crack growth rates were measured by striation counting. Scratches reduced aluminium fatigue life under tensile and bending load up to 97.8% due to multiple cracks nucleation at their roots. Short cracks, nucleated from sharp scratches coalesced to form unique elongated cracks growing through sample thickness. Cracks initiated from scratches were typical short cracks, growing faster than conventional long cracks. Despite the different scribing process, fatigue data of regular diamond tool cut scribes can be used to conservatively predict life reduction owing to ploughed in-service scribe marks on fuselage joints. FE analyses on scribed samples and the fatigue life prediction models are described in Part II of this paper.

Keywords: Notch fatigue; scratches and scribe marks; small cracks; fractography; striations

Nomenclature

a	= crack length measured from the scribe root
d	= scribe depth
da/dN	= fatigue crack growth rate
E	= Young's modulus
K_t	= stress concentration factor ($\sigma_{22}^{root}/\sigma_{max}$)
N^{tot}	= total fatigue life (cycles)
N_{un}^{tot}	= total fatigue life of unscribed samples (cycles)
R	= fatigue loading stress ratio ($\sigma_{min}/\sigma_{max}$)
t	= sample thickness
ϵ_f	= elongation at failure
θ	= scribe included angle
ν	= Poisson's ratio
ρ	= scribe root radius
$\sigma_{0.2}$	= yield strength

σ_{22}^{root} = longitudinal stress at the scribe root

σ_{max} = nominal maximum fatigue stress at gauge section

σ_{min} = nominal minimum fatigue stress at gauge section

σ_{UTS} = tensile strength

1. Introduction

Aircraft structures, except for landing gear and engines, are designed following the damage tolerance approach. Catastrophic failures are avoided by designing structures capable of tolerating defects caused by fatigue, corrosion or accidental impacts, until they can be detected and repaired¹. However maintenance operations, if improperly performed, can cause accidental damage. Inappropriate tools or accidental impacts can damage aircraft and initiate widespread fatigue cracks less than a millimetre deep, making structures unable to meet damage tolerance requirements¹.

Interest in maintenance induced damage was recently revived by the discovery of so called *scribe marks* at fuselage joints. *Scribe marks* are multiple scratches introduced on the fuselage skin along longitudinal and circumferential joints by the use of sharp tools during sealant removal process prior repainting²⁻⁵. *Scribe marks* can be metres long and widespread along every fuselage longitudinal and circumferential joint. While scribes have high variability in length and depth their usual cross section shows a rounded V-shape⁵. *Scribe marks*, no deeper than 200-300 μm , located in highly stressed regions where the joint secondary bending is maximum, are capable of simultaneously initiating multiple small cracks along their roots which coalesce forming a wide crack propagating through the panel thickness⁵. Cracks propagating from scribes are difficult to detect during conventional inspections and when they become visible, after few thousand flights, the damage can be so extensive as to render aircraft beyond economic repair².

If the scratch is regarded as a propagating crack, fracture mechanics can be used to calculate the life to failure⁶, but this approach is very conservative as it neglects fatigue cycles to create the crack. The interaction and coalescence of multiple small cracks together with short crack behaviour⁷⁻¹³ invalidates the use of conventional analysis for cracks nucleated from *scribe marks* before they become through thickness cracks. A new analysis method is therefore required, in the frame of damage tolerance philosophy to predict residual service life of scribed structure and define additional inspection and repair programs.

Fatigue crack development from mechanically induced scratches is a notch fatigue problem, where the stress concentrators are several centimetres long but a few tens of microns deep. The two different scales of length and depth, place long superficial scratches in an intermediate position between conventional engineering notches, several millimetres in size¹⁴⁻¹⁹, and small defects the size of the material characteristic microstructural lengths²⁰⁻²². Together

with the stress concentration caused by the scratch geometry, plastic deformation resulting from the scribing process inevitably causes residual stresses and material hardening at the notch root, in turn affecting fatigue crack nucleation and early propagation²³.

Despite their widespread occurrence mechanically produced scratches have received little attention from fatigue workers. According to traditional fatigue life prediction methods based on notch sensitivity factor^{24,25}, many materials are considered insensitive to scratches on components surfaces. More recently, experimental evidence showed that the presence of mechanically machined scratches had significant impact on fatigue life of aluminium²⁶⁻²⁹ and steel³⁰ components.

Previous investigations on fatigue behaviour of scratched components fall short of providing a detailed explanation of mechanisms involved in crack development from scratches. This research aims to investigate fatigue crack initiation and growth from mechanically machined scratches in clad and unclad 2024-T351 aluminium alloy sheets. The main objective is to characterise the effect of mechanical defects, such as surface scratches, on fatigue life of aluminium samples, providing a background to predict residual service life of aeronautical structures containing *scribe marks*. The influence of scratch geometry on fatigue cracks developing from scratches was isolated from the effects of plasticity and residual stress induced by the scribing process. A detailed analysis of the impact of plasticity and residual stress introduced by the scribing process on fatigue performance of scratched components can be found in³¹. Fatigue tests were conducted on both clad and unclad 2024-T351 aluminium samples. After testing fracture surfaces were examined in the SEM to characterise fracture morphology and to determine crack growth rates from striation spacing measurements. Stress fields and plastic zones at the scratch root were analysed using elastic-plastic finite element models to assess the local stress concentration effect on crack nucleation and early propagation. Experimental and finite element results were used to develop a model for predicting fatigue life of scribed structures and the scratch sensitivity of aluminium structures. FE analyses and the prediction model development are described in Part II of this paper.

2. Experimental procedures

2.1. Material and experiment preparation

The material studied was the aluminium-copper alloy 2024-T351 of which fuselage panels and joints of the majority of civil aircraft in service are made. Table 1 shows its specified chemical composition. The material was supplied as 2 mm thick rolled sheet clad panels in T351 temper condition³³. Unclad 2024-T351 aluminium alloy, was produced by stripping the cladding using chemical milling. That process reduced the thickness to nearly 1.67 mm. Metallographic

examination of clad and unclad materials showed a pancake shape grain structure typical of rolled sheets with grains elongated along the rolling direction L. Grains were approximately 150-200 μm long along rolling direction L, 80-100 μm on transverse direction T and 20 μm in the thickness direction S³⁴. No grain structure was visible inside the pure aluminium clad layer. An average clad depth of 70-80 μm , that is around 3.5% of the whole thickness, was measured on clad 2024-T351 aluminium panels using optical microscope³⁴.

Table 1 Specified chemical composition of Al 2024-T351 (wt%)³².

Fig. 1 Sample geometries for fatigue testing under tension (a) and 4 point bending (b) (dimensions in mm).

Table 2 Mechanical properties of 2424 sheet in the transverse direction LT.

Cracks developed from *scribe marks* at fuselage joints under the combination of fatigue tensile load and secondary bending caused by the joint eccentricity⁵. The effects of pure tension and pure bending loading on crack development from scribes were examined separately. were machined from clad and unclad 2024-T351 sheets to The geometries of tension and bending samples is shown in Fig. 1. A dogbone specimen with continuous radius between ends was chosen for pure tension (Fig. 1a) while a simple rectangular sample (Fig. 1b) was used to perform 4 point bend tests. A scribe was cut across the entire gauge section of the samples perpendicular to the load direction (Fig. 1). The gauge section width was 80 mm to accommodate long scratches representative of service *scribes*. Samples were machined with the rolling direction parallel to the scratch line (Fig. 1), consistent with the material orientation in longitudinal fuselage joints³⁴. Tensile and bending loads were therefore applied along the LT, transverse direction. Table 2 lists the mechanical properties of clad and unclad alloys measured along this direction.

Scribe section and depth in the test samples had to be regular and controllable. Micro notches of rounded V section, with depth (d) between 25 and 185 μm , were cut across the entire gauge width in bending and tension specimens (Fig. 1) using a diamond tipped tool mounted on a precision planing machine³⁴. Three different cross sections, characterised by root radii (ρ) of 5, 25 and 50 μm , were machined, while the included angle (θ) of the V was constant at $\theta=60^\circ$. Scribes were produced using cutting rather than scratching process which is more akin to ploughing, in order to minimise introduction of plasticity and residual stress around the scribe. These local changes would affect crack development at the scribe root and had to be minimised to investigate the relation between the scribe geometry and fatigue life. The process produced rounded V-sections tens of microns deep with regular and controllable cross sections. Two examples of the cross sections produced are shown in Fig. 2. After scribing all samples had their depth measured

optically and selected specimens had the notch shape examined along the entire gauge length by a scanning confocal microscope³⁴. Depth was kept within 6% of its nominal value across the 80 mm width while maximum percentage errors from nominal root radius and open angle were respectively 8% and 2%. Synchrotron X-ray diffraction and nanoindentation measurements on selected scribes, showed negligible levels of tensile residual stresses and work hardening in the material around them²³. Such measurements, together with the absence of material piling up at the scribe flanks (Fig. 2), demonstrates the pure cutting nature of the scribing procedure.

Fig. 2 Cross section shape of diamond tool machined scribes: 100 μm deep 5 μm root radius scribe (a), 100 μm deep 50 μm root radius scribe (b).

2.2. Fatigue testing

Tension and 4 point bend samples were tested under constant amplitude cyclic load control with $R=0.1$ and maximum stress of $\sigma_{max}=200$ MPa at the gauge section. The σ_{max} of 200 MPa was selected as on unscribed samples it gave fatigue lives comparable to those of tested panels and joint coupons cut from retired medium-range aircraft ($2 \cdot 10^5$ flights). In the case of 4 point bend loading the nominal stress condition referred to the surface stress at the gauge section. The nominal stress was defined as the stress which the gauge section would withstand, according to the San Venant's beam theory, if the material was linear elastic³⁴.

Tensile tests were performed at 10 Hz at 20 in lab air. A total of 49 tensile specimens were tested with a combination of five different scribe depths (25 μm , 50 μm , 100 μm , 150 μm , 185 μm) and three root radii (5 μm , 25 μm , 50 μm) on clad and unclad samples. Each test was duplicated apart from scribes 25 μm deep or with 25 μm root radii where only a single specimen was tested³⁴. 4 point bending tests were carried out under the same conditions but at a test frequency of 1 Hz because of the large displacements incurred under the loads required to achieve 200 MPa surface stress. Fig. 3 shows a sketch of the rig used for 4 point bending tests. Sample anticlastic curvature was inhibited by rig configuration to simulate the constraint exerted by rivets on fuselage jointed panels. 26 clad and unclad bending specimens containing scratches with root radii of 5 μm and 50 μm and three depths (50 μm 100 μm and 185 μm) were tested, duplicating each test. Pristine specimens were tested in tension and bending to have reference lives for comparison³⁴. In all tests the failure criterion was complete sample fracture.

Fig. 3 sketch of 4 point bending rig (dimensions in mm).

2.3. Fractography and crack growth measurements

Fracture surface observation was carried out post testing using a high resolution FEG SEM. Quantitative measurements of initiation sites and final crack size and shape were performed.

Local crack growth rate data were obtained via striation counting assuming, that striations are marks left every fatigue cycle³⁶. Striation spacing was measured at 10-20 locations on cracks at a range of depths along a line intersecting the final crack front at its deepest point³⁴. Pictures were taken at each spot, with magnification up to 130000X, and a total of 3 striation spacing measurements performed for each crack depth. A total of 8 tension samples, 4 clad and 4 unclad, containing respectively 185 μm and 50 μm deep scratches with 50 μm and 5 μm root radius were analysed. Only 4 bending specimens had their striation spacing measured: a clad and an unclad 185 μm deep 5 μm root radius scribed sample, a 185 μm deep 50 μm root radius and a 50 μm deep 5 μm root radius scribed unclad specimens.

3. Results

3.1. Fatigue test results

Fig. 4a and b show tension and bending fatigue lives plotted against scribe depth and root radius for clad and unclad specimens. Fatigue lives of pristine samples are plotted with zero notch depth. All scribed samples failed from fatigue cracks initiated at the scribe root apart from an unclad tension sample with a 25 μm deep, 50 μm root radius scribe that after nearly $8 \cdot 10^5$ cycles had the test stopped. Moreover clad specimens tested in bending containing 50 μm deep, 50 μm root radius scribes failed at locations other than the scribe line.

Pristine samples failed via fatigue cracks located at the minimum gauge section. Specimens containing 25 μm deep scribes with 25 μm and 50 μm root radii had lives comparable to pristine samples. Fig. 4 shows that introduction of scribes caused reduced variability in fatigue lives compared to that observed for pristine samples under the same nominal stress condition^{37,38}. Samples tested in bending showed a larger variability compared with tension tests. Fatigue life decreased with increasing scribe depth for a given root radius and reducing the root radius with a fixed depth had the same effect (Fig. 4). Scribes reduced the fatigue life under tensile load by up to 97.7% for the deepest and sharpest scribes (185 μm deep 5 μm root radius scribe). Even shallow scribes such as 25 μm deep and 25 μm root radius resulted in a 30% life reduction for clad tension samples (Fig. 4a). Fatigue lives of bending samples were on average a factor of 3 longer than the corresponding tension ones (Fig. 4b). Clad samples showed fatigue lives on average 40-50% longer than unclad specimens.

Fig. 4 Sample fatigue life as function of scratch depth and root radius under tension (a) and 4 point bending (b).

3.2. *Fractography observations*

Multiple fatigue cracks nucleated at notch roots along the entire scribe length, growing through thickness in all samples (Fig. 5a). Table 3 lists the fracture front morphology of tension clad samples. The number and linear density of crack nucleation sites along scribe roots increased for deeper notches with smaller root radii (Table 3). Multiple cracks coalesced during propagation, forming fracture surfaces with different shapes. Scribes deeper than 50 μm under tensile loading developed a single elongated fracture front covering the entire sample width whereas scribes shallower than 50 μm showed fracture surfaces made of multiple thumbnail and corner cracks (Table 3 and Fig. 5c). On samples with 25 μm and 50 μm root radii, the elongated crack fronts showed arrays of parallel coalescence steps (coalesced front), suggesting that the fracture front had been made of cracks growing on different planes prior to coalescence (Fig. 5b). Cladding seemed not to influence the fracture morphology as clad and unclad samples containing the same scribes showed similar crack morphology. Under bending loading, the transition between multiple crack and elongated fracture fronts occurred at scribes 100 μm deep³⁴. In specimens showing multiple crack fronts the crack causing sample failure was at the specimen edge which was also the starting location of unstable propagation in single crack fronts.

Table 3 Fracture front morphology of tension clad samples.

Fig. 5 Fracture surface morphology: thumbnail crack at the root of 25 μm deep 50 μm root radius scribe in tension clad specimen (a), elongated crack front with coalescence steps at the root of 185 μm deep 50 μm root radius scribe in a tension clad sample (b), multiple thumbnail crack fronts at the root of 50 μm deep 50 μm root radius scribe in a tension unclad sample (c).

Fatigue cracks generally nucleated in tension and bending from intermetallic particles, voids and superficial damages at the scribe root. Fig. 6a shows a surface crack nucleated from intermetallic particles at the 50 μm root radius of a 50 μm deep scribe in tension unclad sample. Nucleation occurred slightly earlier at sample edges, where the deepest crack fronts were observed³⁴. At roots of small scribes completely embedded into the clad layer there were no substantial changes from the nucleation mechanisms, taking place in the 2024-T351 aluminium alloy substrate. However nucleation from intermetallic particles was not observed from sites inside the clad layer, as consequence of its low content of inclusions and intermetallic particles³⁹.

Where crack nucleation took place, an initial uneven region of fracture a few microns deep, characterised by micro-cliffs separated by regions with irregular appearance was observed (Fig. 6b and c). Fracture surfaces, produced by early crack growth in 2024-T351, showed a jagged aspect with arrays of lamellar features forming micro steps parallel to the local growth direction (Fig. 6a and b). The lamellae were formed by crack growth along different planes of the same slip system inside a grain and changed their orientation and planar slope at grain boundaries because of the tilt angle between favoured slip systems in adjacent grains⁴⁰. Different crack propagation plane orientations in diverse grains are pointed out by variations of surface brightness in Fig. 6a and b. On the whole cracks remained perpendicular to the loading direction but locally grew along crystallographic planes (stage I-like⁴¹). If scribes were completely embedded into cladding, initial crack growth was into pure aluminium. Generally propagation through cladding of small thumbnail cracks was characterised by a geometric structure composed of regular facets (Fig. 6c), typical of crystallographic stage I fatigue crack growth⁴². The growth plane orientation changed at grain boundaries. As soon as the crack approached the substrate the facets were replaced by the ‘feathery’ corrugated features, as those typical of crystallographic stage I growth in 2024-T351 aluminium alloy (Fig. 6c). Crack growth in the substrate was recognisable by the development of the peculiar lamellar arrays (Fig. 6c). For large thumbnail or elongated through sample width cracks, growth into cladding resulted in a structure insensitive amorphous fracture surface, perpendicular to the loading direction³⁴. Propagation returned to microstructure sensitive once the crack grew into the substrate.

Early crack growth from scribe roots showed a strong microstructure sensitivity. Despite different scribe geometries and presence or absence of cladding, transgranular stage II growth (Fig. 6d) developed when cracks reached depths from the sample surface of 180-235 μm under tensile and 240-285 μm , under bending loads³⁴. Stage II crack growth was characterised by multiple raised plateaus, where fatigue striations were detected (Fig. 6d). All samples failed showing a final ductile fracture characterised by void coalescence (Fig. 5 and Fig. 6).

Fig. 6 Fatigue crack development in scribed samples: thumbnail crack nucleation from inclusion and early propagation at the root of 50 μm deep 50 μm root radius scribe in unclad tension sample (a), microstructure sensitive crack growth in 50 μm deep 5 μm root radius scribed unclad tension specimen (b), crack growth through cladding in 25 μm deep 5 μm root radius scribed clad sample (c), crack growth through different stages in 185 μm deep 5 μm root radius scribed unclad tension specimen (d).

3.3. Crack growth rate measurements using striation counting

Striation spacing measurements were carried out from the scribe root up the crack depth where void coalescence occupied nearly 50% of the fracture surface³⁴. No striations were detected in the region of microstructure sensitive

propagation. Fig. 7 shows crack growth rates, deduced from striation spacings of all the tension and bending samples examined, plotted against the distance from the scribed surface $a+d$ normalised by specimen thickness t . The normalised depth $(a+d)/t$ takes into account the sample finite thickness effect on crack propagation rate. Specimens are indicated in Fig. 7 using a nomenclature where the first letter specifies the loading condition (T=tension, B=bending), the second the material (U=unclad, C=clad) and the following numbers define respectively scribe depth and root radius in μm^{34} . Measured growth rates ranged from a minimum value of $0.032 \mu\text{m}/\text{cycle}$ up to a maximum of $0.680 \mu\text{m}/\text{cycle}$. Crack growth rates of tension specimens were well correlated by normalised depth for all scribe geometries, cladding state and crack front shape (Fig. 7). Growth rates under tensile load were an exponential function of increasing normalised crack depth.

Under bending load growth rates were approximated by a third degree polynomial function of normalised crack depth following an S-shaped trend in all samples (Fig. 7). For normalised depth smaller than 1.5, cracks propagated at comparable rates under tensile and bending loads. As soon as cracks became bigger, bending growth rate became up to 60% slower than the tension one. For bending loads normalised crack depth did not unify growth rates in different scribed samples as accurately as for tensile loading. In particular propagation rates from $50 \mu\text{m}$ deep, $5 \mu\text{m}$ root radius scribed sample were still smaller than those from other bending samples even after considering the finite thickness effect (Fig. 7). The different crack fronts composed of multiple cracks rather than the elongated ones exhibited by the other bending samples was thought to be the main cause of growth rate reduction.

Fig. 7 Experimental crack growth rate in tension and bending samples.

4. Discussion

4.1. Effect of scribes on fatigue life

Stress concentration factors, K_t , for each scribe geometry and loading mode were calculated by performing two-dimensional linear elastic finite element analysis. Details of the calculation are given in ⁴³. Table 4 lists gross elastic K_t values of each scribe geometries under tensile and bending loads. No distinction was made between concentration factors on clad and unclad samples as the elastic properties of substrate and cladding materials were identical and the small variation caused by the different sample thickness was neglected⁴³. Because of the small size of scribes compared to the sample thickness ($d/t < 1/10$), K_t was mainly regulated by the notch aspect ratio ρ/d as for V-notches in semi-infinite plates⁴⁴.

Table 4 Stress concentration factors of scribes under tensile and bending load.

Scribe fatigue lives normalised with respect to lives of unscribed specimens, N^{tot}/N_{un}^{tot} are plotted against stress concentration factors in Fig. 8a to isolate the scribe geometry effect on fatigue. Irrespective of loading mode and cladding status, normalised fatigue lives of samples with the same root radius all lie on the same curve. There are separate data trends for different root radii, demonstrating the well-established inability of elastic K_t alone to characterise the effect of notches on fatigue life^{24,25}.

The exception to the trend is for 25 μm deep, 5 μm root radius scribes ($K_t=5.88$), which showed a smaller life reduction for clad than for unclad tension samples (Fig. 8a). The effect of scribes on fatigue life is therefore independent of loading mode and is reduced by cladding only for scribes with their root embedded within the soft layer. This smaller life reduction was thought to be caused by notch root blunting in the soft aluminium. Blunting was believed to be hampered by the constraint exerted by the nearby harder substrate for 50 μm deep scratches, as their normalised lives were the same in both clad and unclad samples. 50 μm deep, 50 μm root radius scribes ($K_t=2.96$) generated fatigue fracture in unclad bending specimens but not in clad ones (Fig. 4 and Fig. 8a). K_t values ≤ 2.43 in tension and ≤ 2.96 in bending had no effect on fatigue life and represent a threshold condition. Scribes with K_t less than this (Fig. 4) were found to be as deep as the size of the inclusion clusters (23-60 μm) which nucleated propagating fatigue cracks in pristine samples³⁴

Cladding and bending loading modes both shifted sample fatigue lives to greater number of cycles compared to the lives of corresponding tension specimens (Fig. 4). For a given surface stress, a longer crack nucleation period is commonly observed in bending fatigue and is generally ascribed to the smaller volume of highly stressed material in bending stress gradient⁴⁵. This cause seems unlikely in the current tests as the root stress volume in tension and bending will not be significantly different. An alternative explanation for the increased bending lives is the crack propagation from scribes which had growth rates up to 85% slower than in tension (Fig. 7). As well as increasing the fatigue life of scribed samples, cladding increased the life of pristine specimens by nearly 43% (Fig. 4). This behaviour was inconsistent with data reported in prior literature where the clad layer is reported to have a large detrimental effect on S-N curve of aluminium alloys. This was interpreted as being due to the plastic shake down of the soft pure aluminium which promoted crack nucleation^{46,47}. In the current work work fatigue life of clad specimens was thought to be regulated not by crack nucleation but by the increased cycles required for a crack to penetrate into the substrate material⁴⁷. The longer life of unscribed clad samples was ascribed to fatigue crack nucleation from subsurface inclusion clusters, increasing the initiation life³⁴. The effect of cladding and bending load on local scribe stress fields and its implications in initiation and propagation lives are discussed in Part II of this paper.

Fig. 8 Effect of the scribe geometry on total fatigue life of aluminium samples (a) and on nucleation site density and fracture morphology of clad specimens (b).

4.2. Crack development from scribes

Scribes reduced specimen fatigue lives via initiation of multiple fatigue cracks at their roots where raised stress caused dislocation motion and plasticity, which in turn are responsible for crack formation. Similar multiple nucleation processes have been observed in other investigations on scratches^{5,26}. The scribe root will intersect different grains of different orientations and their variability in orientation will give a range of values of critical resolved shear stress for slip, determined by the value of the Schmid factor in each grain. Crack nucleation will also be promoted by the presence of inclusions of a range of diameters within the grains and their location with respect to the notch root. For a given scribe geometry cracks will initiate first and grow fastest in stage I single slip growth in grains which have the largest inclusions nearest the notch root and the largest value of the Schmid factor (0.5).

Scribe geometry regulated the number of crack nucleation points per unit length of scribe root, (Table 3). Fig. 8b shows the linear density of nucleation sites as a function of K_t in clad samples. Specimen fracture front morphology is indicated as well in Fig. 8b. Unclad samples showed a similar trend to that in Fig. 8b. The linear density of crack nucleation points increased with K_t . Only scribes with 25 μm depth in tension and 50 μm depth in bending deep, with 5 μm root radius deviated from this trend (Fig. 8b).

For scribes with $K_t < 4.08$, nucleation points had a density of < 2.63 1/mm (Fig. 8b). Crack nuclei were more than 380 μm apart on average, generating fracture fronts made by multiple superficial flaws. If $4.08 \leq K_t \leq 8.07$, resistance to dislocation motion was overcome over an increased number of initiation sites generating a nucleation site density from 2.63 1/mm to 7.54 1/mm (Fig. 8b). Crack nuclei were 130-180 μm apart and coalesced in the early stage of their propagation to form a single elongated coalesced fracture front as for 185 μm deep 50 μm root radius scribes. Coalescence steps were mainly developed from 25 and 50 μm root radii scribes, where larger radii promoted crack nucleation and early growth on parallel offset planes. For sharp scribes with $K_t > 8.07$, as 185 μm deep 5 μm root radius ones (Fig. 8b), a nucleation site was activated on average every 100-130 μm along the scribe root (linear density > 7.54 1/mm). The nucleation process was so spread that a crack few microns deep but lengthened along the entire scribe length was thought to develop at the scribe root.

There was a correlation between the fracture front morphology and the fatigue life of scribed samples as shown in Fig. 8a. Scribes producing multiple crack fronts had reduced fatigue lives as small as 14% of those of pristine samples. Smaller lives were reached only by developing elongated crack front with or without coalescence steps (Fig. 8a). At

normalised fatigue lives around $N^{tot}/N_{un}^{tot}=14\%$ bending samples developed multiple crack fronts while tension ones generated single fracture fronts.

Early crack growth from scribe marks was sensitive to material grain structure in both cladding and substrate. Crack propagation in cladding showed regular facets typical of crystallographic stage I growth (Fig. 6c) or amorphous structure-insensitive fracture surfaces depending on the crack size. A possible explanation for such different behaviour could be imputed to different constraints exerted along crack fronts⁴⁸ or to a diverse crack growth rate. The microstructural nature of early crack propagation from scribes was consistent with the formation of multiple small cracks at the scribe root which afterwards coalesced to form larger fracture fronts. In fact the congruence constraint exerted on a crack encompassing many grains promotes the development of structure insensitive stage-II growth⁴⁸. The transition to stage II growth in scribed samples seemed to be regulated by the crack tip plastic zone rather than by the notch plastic zone as the transition crack depth was independent of scribe geometry being regulated only by loading condition.

Fig. 9 Comparison between measured growth rates of cracks from scribe marks and calculated rates for single edge notch cracks under tensile and bending loads as function of normalised distance from the sample surface.

Ductile striations were clearly visible only when transgranular stage II growth developed, that is 50-100 μm and 100-190 μm from the scribe root under tensile and bending loads respectively. Scribe geometry and cladding did not affect crack growth data as growth rates of different samples had a single trend line when plotted against normalised crack depth $(a+d)/t$ (Fig. 7). The effect of the thicker clad samples and of notch depth was to modify the sample net ligament length and the consequent finite thickness influence exerted on cracks. Fig. 9 shows a comparison between crack growth rates measured by striation counting and those calculated for single edge notch cracks using long crack growth curve⁴⁹ on tension and bending samples. The long crack shape was selected as two-dimensional through-width edge cracks. These have the highest growth rate for a given crack depth. Cracks nucleated from scribes showed typical short crack behaviour, growing up to 10 times faster than long cracks with the same normalised depth. Measured growth rates merged with long crack data for depths close to the critical value for unstable fracture Fig. 9. Bending samples showed striation growth rates smaller than long crack ones for cracks approaching the sample edge. Such anomalous behaviour was thought to be caused by the development of a plastic hinge in the sample net ligament under 4 point bending load, which reduces the crack driving force³⁴.

4.3. Diamond tool scribes vs. simulated in-service scribes

Diamond cut scribes were not representative of in-service scratches, produced by sealant removal from fuselage joints. Even with similar geometry, in-service scratches produced by ploughing had considerable plasticity and residual stress fields in and around the notch root, altering the fatigue crack development^{31,52,53}.

The effect on fatigue life of scribes similar to in-service ones was analysed to assess the relevance of fatigue data generated on diamond cut scribes to aircraft service. In related work, simulated in-service scribes were introduced into dogbone samples (Fig. 1a) using plastic scrapers, steel knife blades, aluminium alloy blades and high strength steel tools^{31,52,53}. It was reported that plastic scrapers, recommended for sealant removal, were not able to scratch the surface of clad and unclad aluminium alloy samples⁵². Samples were subsequently fatigued under the same conditions as the diamond cut scribes^{31,52,53}. Fig. 10 shows fatigue lives of simulated service scribes and diamond cut ones, plotted against scribe elastic K_t . Runout samples are indicated by arrows, open symbols specify specimens failing at their edge rather than at the scribe root. Fatigue test data reported in figures 4 and 8 were compared to data from Morency⁵¹, testing 5 μm root radius scribes machined by a damaged diamond tool and Tizard³¹, who fatigued samples scribed by an high strength steel tool (Fig. 10a). For clad samples, fatigue data from simulated service scribes, obtained by Irving et al.⁵⁰, using an high speed steel tool, Walmsley⁵², by plastic and aluminium scrapers, Jozelech⁵³, using aluminium tools and Stanley knives, and Morency⁵¹ are used for comparison (Fig. 10b).

Fig. 10 Effect of diamond tool and like in-service scribes on fatigue life of unclad (a) and clad (b) samples.

Generally simulated service scribes were less damaging for clad and unclad 2024-T351 aluminium alloy sheets than scribes cut by diamond tools. All the fatigue life data of samples with simulated service scribes, including also scribes machined by the damaged diamond tool, were greater than those with diamond cut specimens (Fig. 10). Simulated scribes were more averse than diamond tool ones to initiate fatigue cracks. Simulated scribes with $K_t \leq 6$ for unclad³¹ and $K_t \leq 4-5.5$ for clad samples^{46,48} had the same fatigue lives as pristine samples (Fig. 10).

Nanoindentation measurements on simulated service scribes showed increased hardness around their profiles compared to diamond scribes (Fig. 11) and also the existence of compressive residual stresses close to the material yield strength at the notch roots³¹. The inelastic deformation on simulated scribing gave rise to local hardening (Fig. 11) and plasticity-induced compressive residual stresses. These processes are largely absent in diamond cut scribes.

The increase in material hardness and the compressive residual stresses are believed to be responsible for the improved fatigue performances of simulated service scribes³¹. Crack initiation and early propagation at the scribe root, will be retarded making the total lives of service scribed samples longer than those of diamond tool ones³¹. A fatigue life prediction method based on the experimental data of diamond tool scribed samples will give conservative lives when applied to scratches found on in-service aircraft.

Fig. 11 Material hardness along the centreline of diamond cut and simulated service scribes measured by nanoindentation³¹.

5. Conclusions

- Diamond cutting tools with root radii of 5, 25 and 50 μm and a face angle of 60° can be used to produce cut scribes in the surface of sheet samples of 2024-T351 of depth between 25 and 180 μm with the above root radii and with minimal associated plasticity.
- Tensile and bending fatigue testing has been performed at 200 MPa, $R=0.1$ on 2024-T351 aluminium samples clad and unclad containing diamond cut scribes. Scribes with elastic stress concentration factors $K_t \geq 2.43$ in tension and $K_t \geq 2.96$ in bending reduced fatigue life by up to 97.8% due to multiple crack nucleation at their roots.
- Scribes with stress concentrations less than $K_t=2.43$ did not initiate fatigue cracks and represent a threshold condition.
- Clad samples showed nearly 50% increased fatigue life compared to unclad specimens with the same scribe geometry. Scribed samples, fatigued under pure bending load, showed the same trend as under tension, but produced lives on average 3 times longer than corresponding tension specimens due to slower crack propagation.
- Post-test fractography revealed that multiple crack initiation occurred from scribes usually from intermetallic particles, defects or favourably oriented grains along the root. The number of crack nucleation sites per unit length of scribe root increased with K_t . For $K_t > 8.07$, the nucleation site density > 7.54 1/mm promoted the development of multiple short cracks which coalesced, during early propagation, forming a single crack along the whole sample width. Scribes with $K_t < 4.08$, had a linear nucleated crack density < 2.63 1/mm, generating fracture surfaces of multiple thumbnail and corner cracks. For $4.08 \leq K_t \leq 8.07$, tension and bending samples showed elongated or multiple crack fracture fronts depending on scribe depth and loading conditions.
- Early crack growth was strongly influenced by material microstructure, despite different notch geometry, cladding and load conditions. The transition between stage I-like and stage II growth seemed to be regulated by the crack tip plastic zone rather than by the notch plastic zone. Scribe geometry influenced only the microstructure sensitive stage I-like crack propagation.
- Crack growth rate was measured performing striation counting on fracture surfaces. Fatigue ductile striations were clearly visible when stage II growth developed (50-190 μm from the scribe root). Cracks propagation in bending

was up to 60% lower than in tension. Cracks nucleated from scribes showed the typical short crack behaviour for the entire propagation stage, growing up to 10 times faster than long cracks with the same size and shape.

- A comparison of fatigue lives of samples with diamond scribes with samples containing simulated scribes showed that simulated service scribes were less effective in producing fatigue cracks. This is attributed to their greater plasticity and compressive residual stress. Fatigue life predictions of service scribes based on experimental data of diamond tool scribed samples are therefore conservative as the scribing process was most damaging.

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Table 1

Material	Si	Fe	Cu	Mn	Mg	Cr	Zn	Ti	Others	
									Each	Total
Al 2024-T351	0.50	0.50	3.8-4.9	0.3-0.9	1.2-1.8	0.10	0.25	0.15	0.05	0.15

Table 2

Al 2024-T351	Young's modulus E [MPa]	Poisson's ratio ν	Yield strength $\sigma_{0.2}$ [MPa]	Tensile strength σ_{UTS} [MPa]	Elongation ε_f [%]
Unclad LT ³⁴	72000	0.33	360	481	19
Clad LT ³⁵	$65500 \leq E \leq 70500$	0.33	280	425	15

Table 3

Sample	Scribe		Fracture front			Nucleation points	
	d [μm]	ρ [μm]	Type	Crack number	Main crack shape	Number	Density [1/mm]
T-C-0-0	-	-	1 elliptical	1	corner	1	0.01
T-C-25-5	25	5	multiple cracks	10	surface	221	2.76
T-C-50-5	50	5	coalesced	1	through	603	7.54
T-C-100-5	100	5	elongated	1	through	681	8.51
T-C-150-5	150	5	elongated	1	through	731	9.14
T-C-185-5	185	5	elongated	1	through	793	9.91
T-C-25-25	25	25	multiple cracks	8	surface	33	0.41
T-C-50-25	50	25	multiple cracks	7	corner	165	2.06
T-C-100-25	100	25	coalesced	1	through	499	6.24
T-C-150-25	150	25	coalesced	1	through	572	7.15
T-C-185-25	185	25	coalesced	1	through	588	7.35
T-C-25-50	25	50	multiple cracks	5	surface	15	0.19
T-C-50-50	50	50	multiple cracks	15	corner	38	0.48
T-C-100-50	100	50	coalesced	1	through	210	2.63
T-C-150-50	150	50	coalesced	1	through	332	4.15
T-C-185-50	185	50	coalesced	1	through	547	6.84

Table 4

Scribe geometry				$K_t = \frac{\sigma_{22}^{root}}{\sigma_{max}}$	
d [μm]	ρ [μm]	θ [$^\circ$]	Aspect ratio ρ/d	Tension	Bending
25	5	60	0.200	5.88	5.77
50	5	60	0.100	8.07	7.76
100	5	60	0.050	11.27	10.42
150	5	60	0.033	13.95	12.34
185	5	60	0.027	15.70	13.44
25	25	60	1.000	3.07	3.01
50	25	60	0.500	4.02	3.86
100	25	60	0.250	5.44	5.01
150	25	60	0.167	6.64	5.84
185	25	60	0.135	7.44	6.32
25	50	60	2.000	2.43	2.38
50	50	60	1.000	3.09	2.96
100	50	60	0.500	4.08	3.74
150	50	60	0.333	4.93	4.31
185	50	60	0.270	5.49	4.64

Fig 1

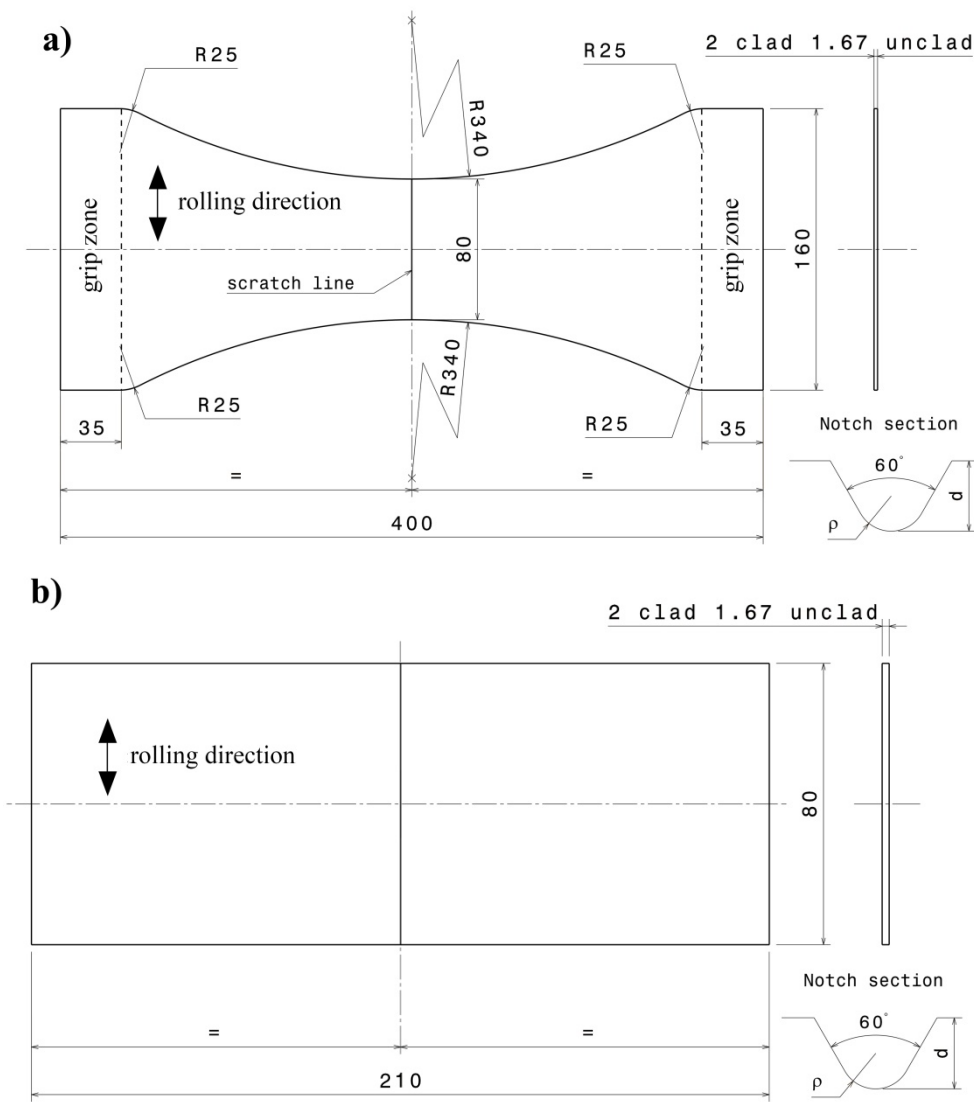


Fig 2

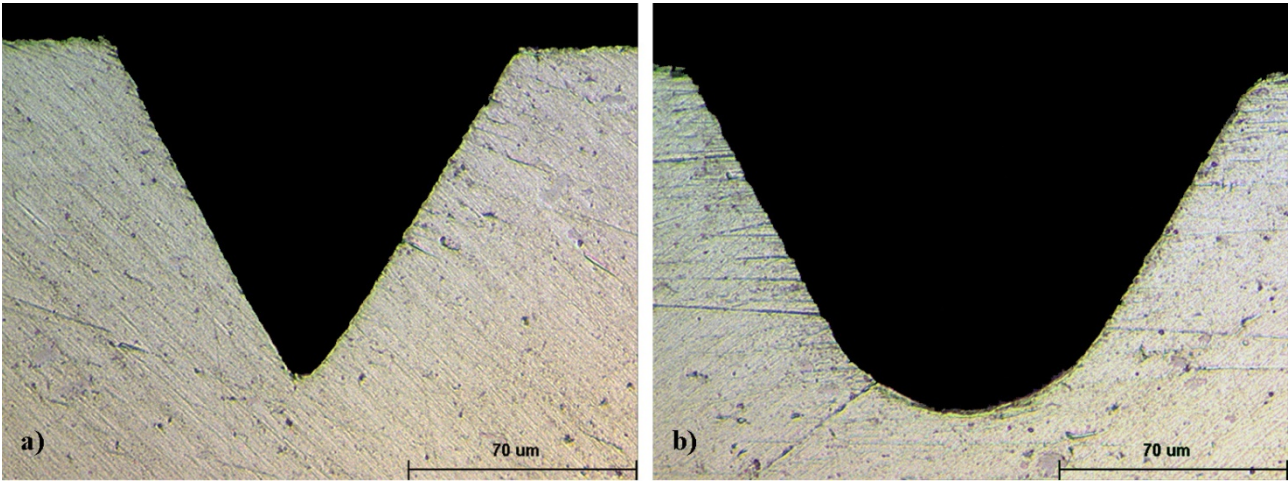


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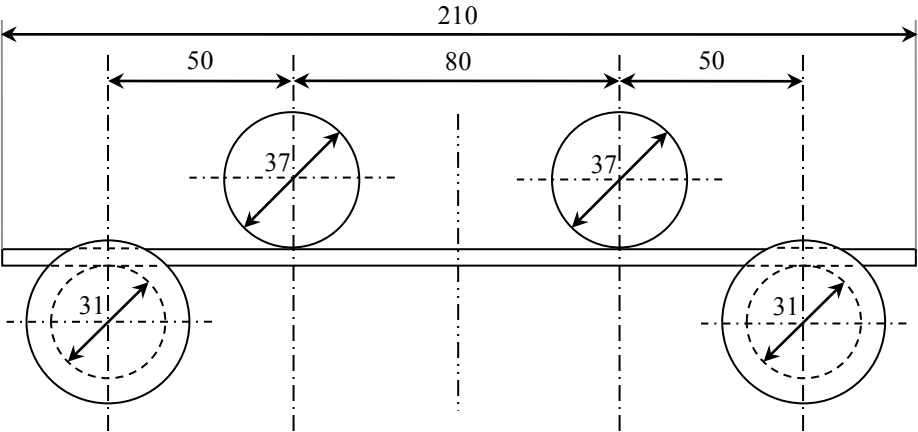


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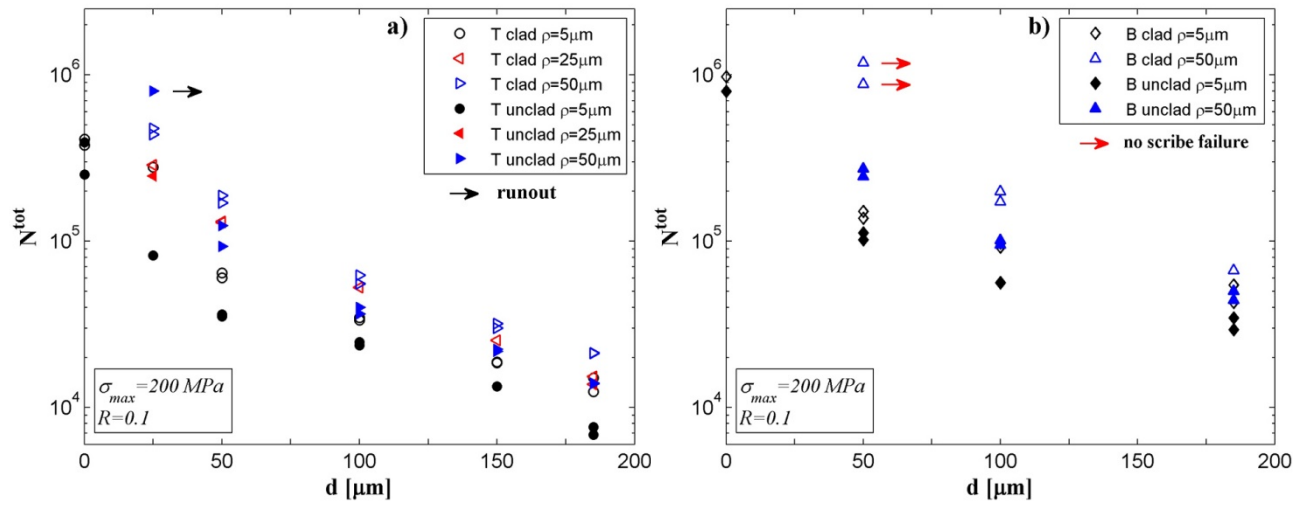


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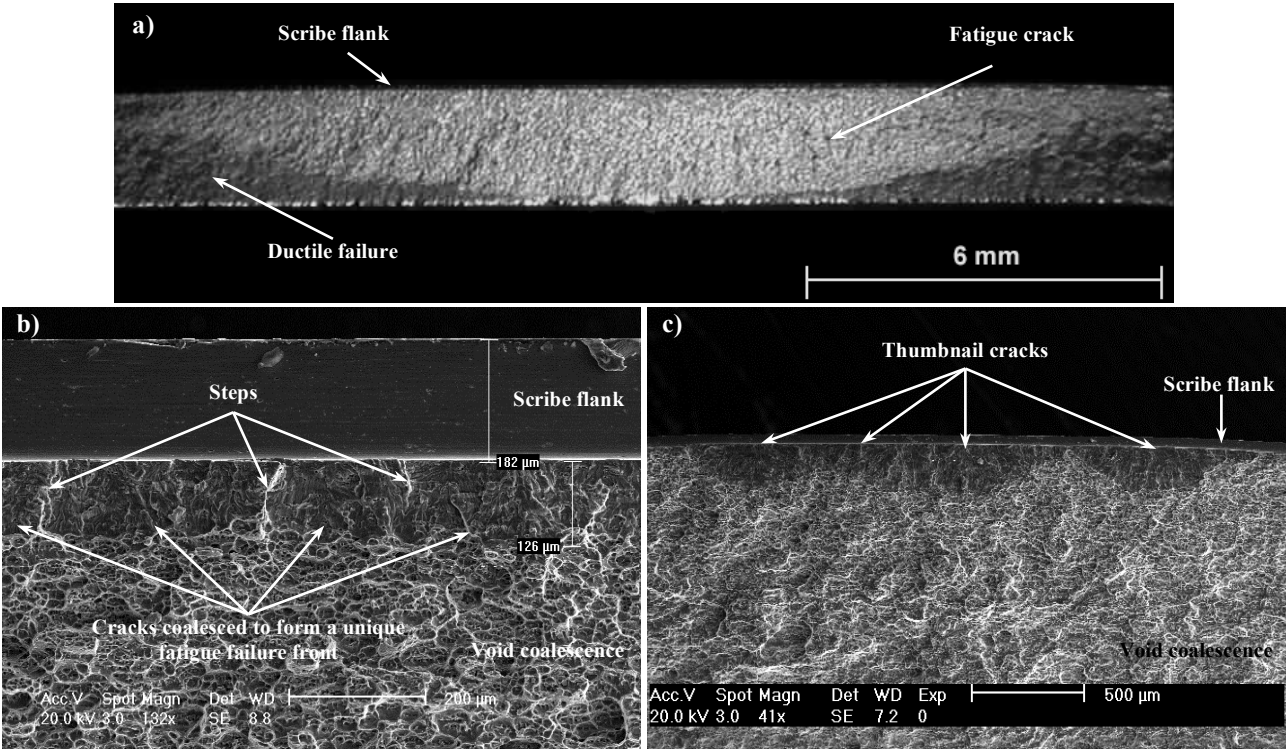


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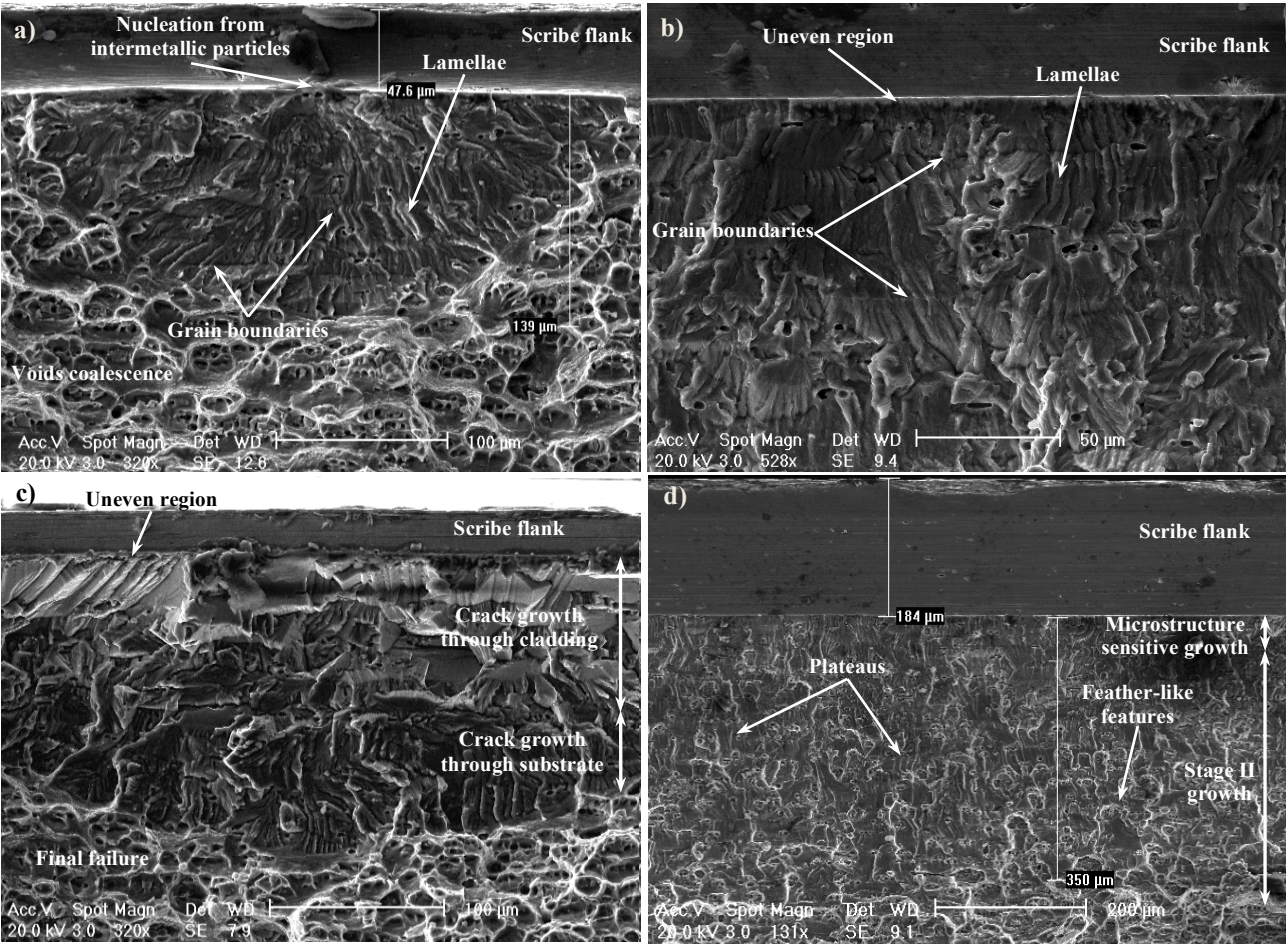


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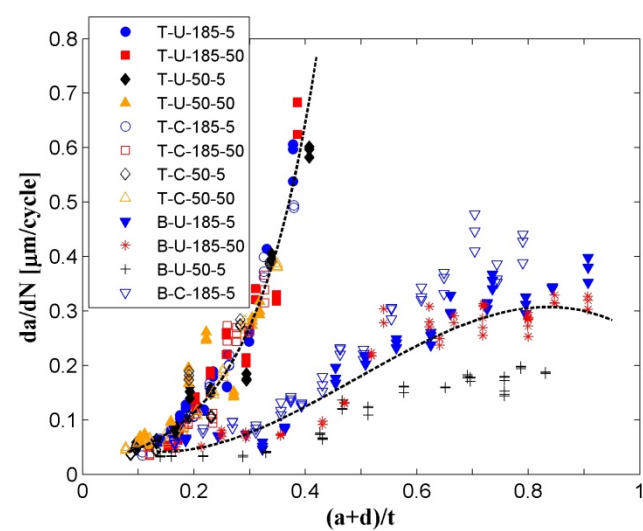


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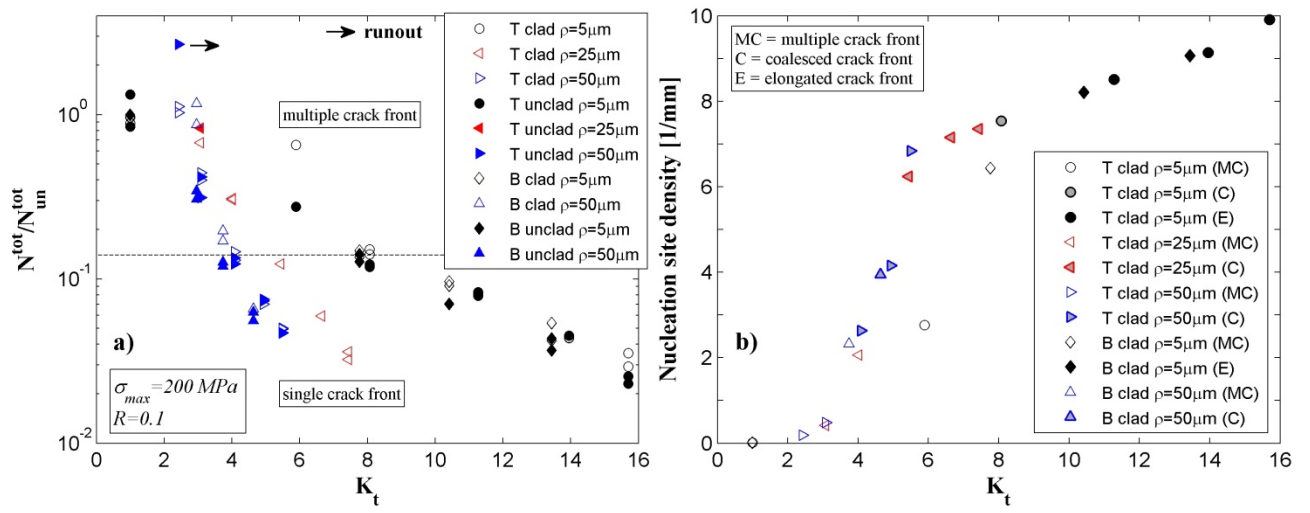


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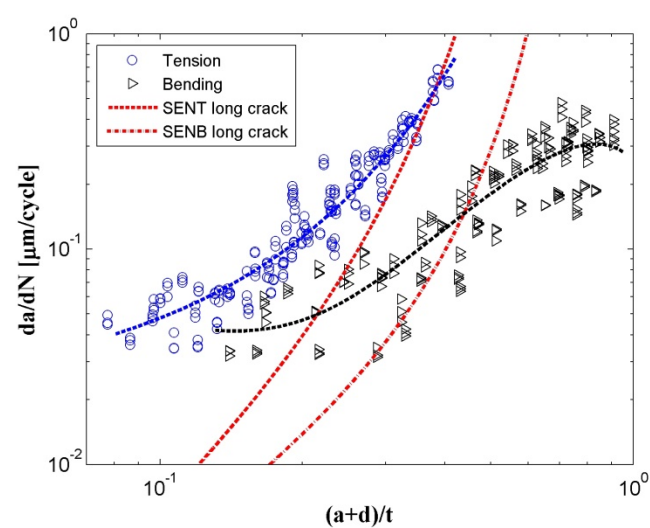


Fig 10

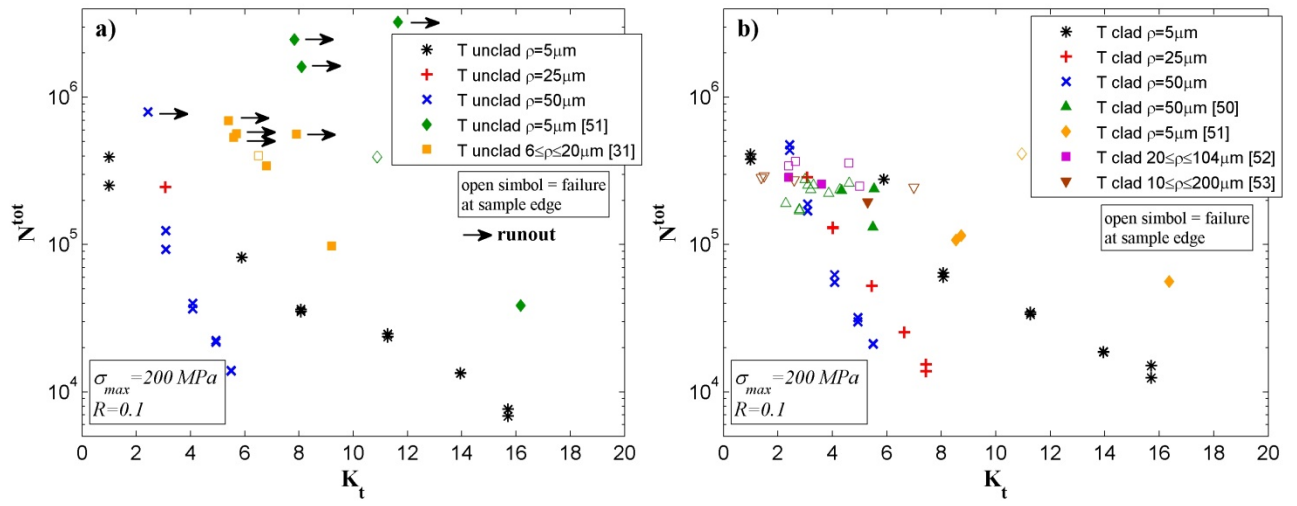
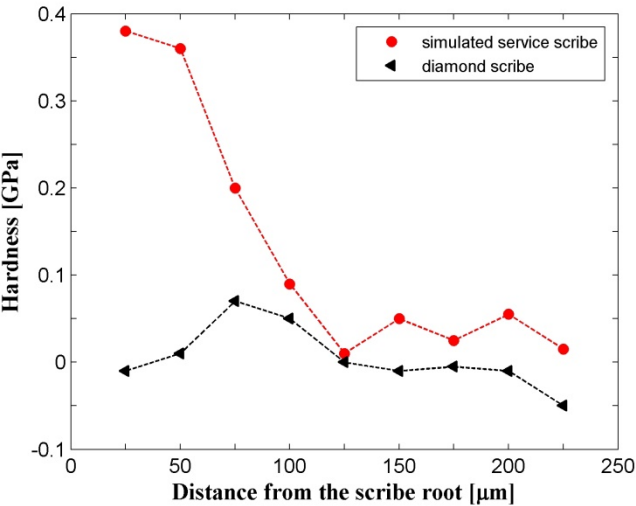


Fig 11



2016-10-27

Development of fatigue cracks from mechanically machined scratches on 2024-T351 aluminum alloy - Part 1: experimentation and fractographic analysis

Cini, Andrea

Wiley

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